# Low-Thrust Many-Revolution Trajectory Optimization via Differential Dynamic Programming and a Sundman Transformation

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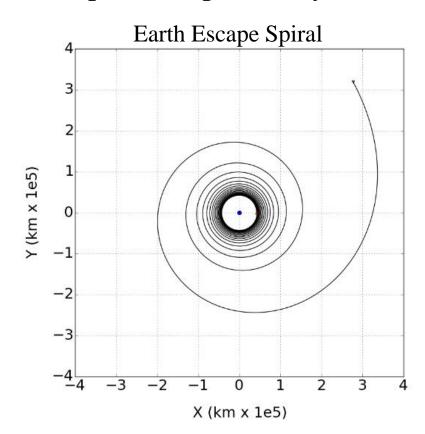
Jacob Englander NASA Goddard Space Flight Center



# How many revolutions?

#### **Planetary**

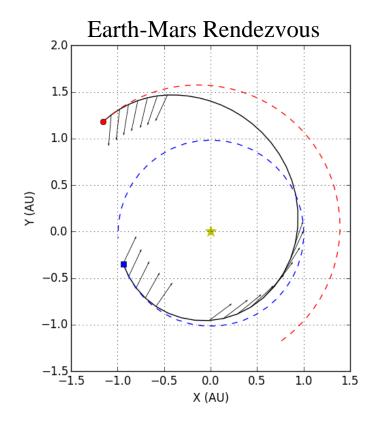
• Long transfer durations with short orbital periods span many revolutions



Number of 'revs': 10s, 100s, 1000s

#### **Interplanetary**

• Slow dynamics compared to control schedule



< 1, 1-10, 10s

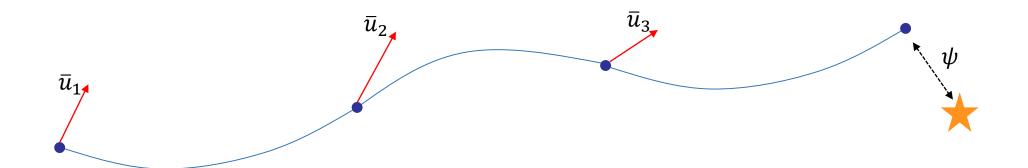


# Historical Approaches

Indirect	Control Laws	Direct		
optimal control theory, apply Euler-Lagrange theorem and solve two point boundary value problem (TPBVP)	set a rule for spacecraft steering – a suboptimal policy that is acceptable by the mission designer	transcribe the trajectory optimization into a parameter optimization problem		
Edelbaum Alfano Kéchichian	Kluever Chang Petropolous	Betts Whiffen Lantoine		

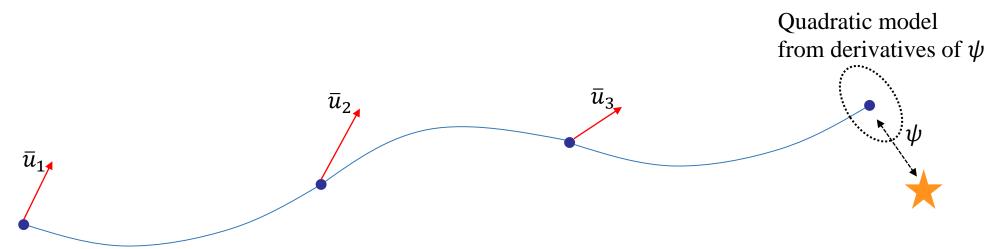


- Hybrid Differential Dynamic Programming
  - introduced by Lantoine and Russell
  - sequence of control updates that minimize quadratic model of *cost-to-go*
  - map derivatives along trajectory with state transition matrix and tensor



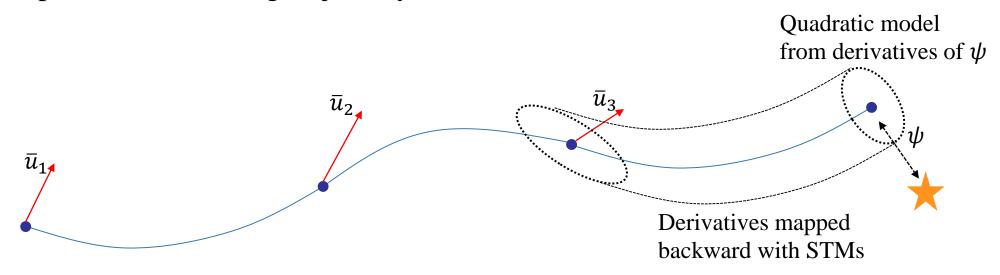


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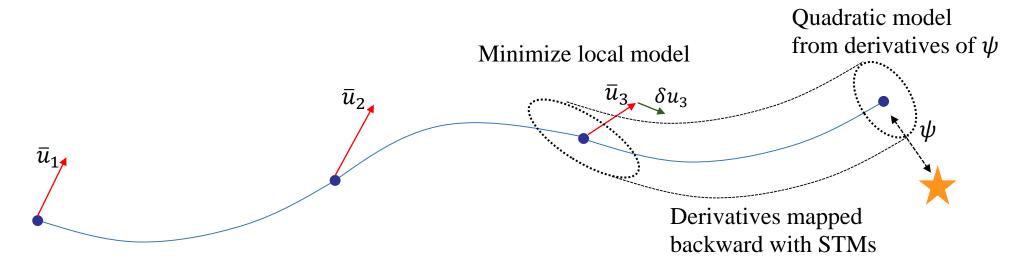


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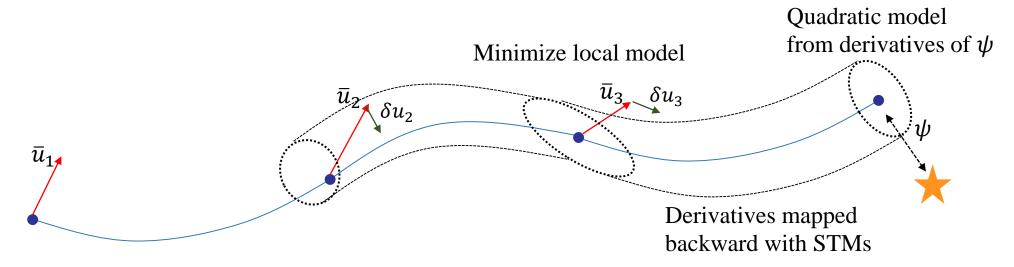


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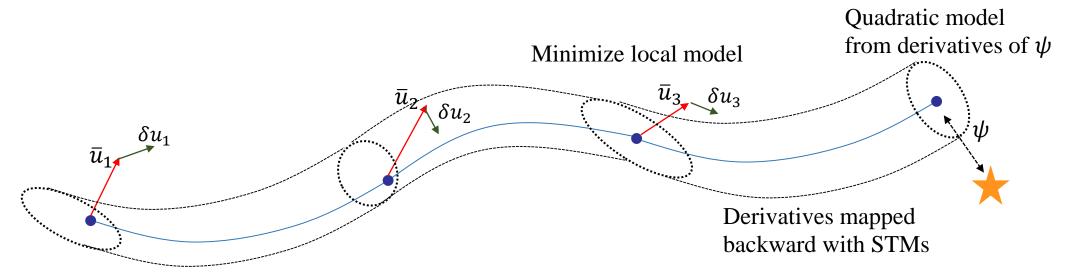


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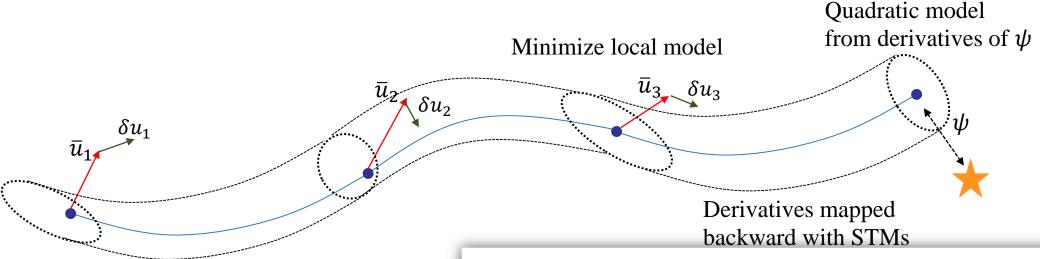


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- Forward pass: evaluate  $\bar{u} + \delta u$  in equations of motion
- Backward sweep: compute each  $\delta u_k$

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- Forward pass: evaluate  $\bar{u} + \delta u$  i
- Backward sweep: compute each

#### See:

Gregory Lantoine and Ryan P. Russell. A hybrid differential dynamic programming algorithm for constrained optimal control problems. part 1: Theory. Journal of Optimization Theory and Applications, 154(2):382-417, 2012.

## The Sundman Transformation

• Change independent variable from time to a function of orbital radius

$$dt = c_n r^n d\tau$$

• Can choose n,  $c_n$ , so that  $\tau$  is an orbit angle

Eccentric Anomaly	Mean Anomaly	True Anomaly		
$dt = \sqrt{\frac{a}{\mu}} r dE$	$dt = \sqrt{\frac{a^3}{\mu}} dM$	$dt = \frac{r^2}{h}dv$		

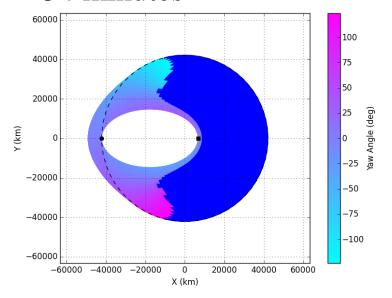
- Equations of motion become  $x' = \dot{x}c_n r^n$
- Discretize in  $\tau$
- Specify  $\tau_0$ ,  $\tau_f$ , rather than  $t_0$ ,  $t_f$ 
  - i.e. specify number of revolutions

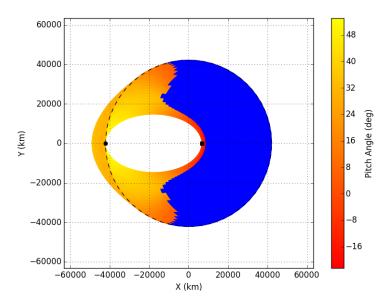
• Track time in the state vector

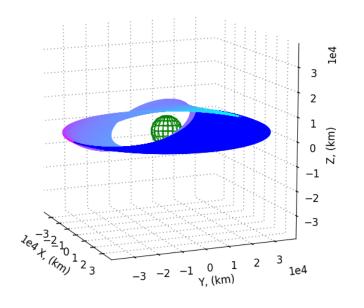
$$x = \begin{bmatrix} t \\ x \\ y \\ z \\ \vdots \end{bmatrix}, \qquad x' = \begin{bmatrix} 1 \\ \dot{x} \\ \dot{y} \\ \dot{z} \\ \vdots \end{bmatrix} c_n r^n$$

- Choose  $\tau = E$ , the eccentric anomaly
- Minimum fuel GTO to GEO in 450.5 revs
- 2-body dynamics
- 135,150 variables

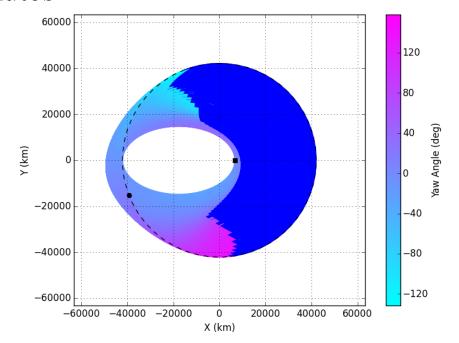
#### • 54 minutes

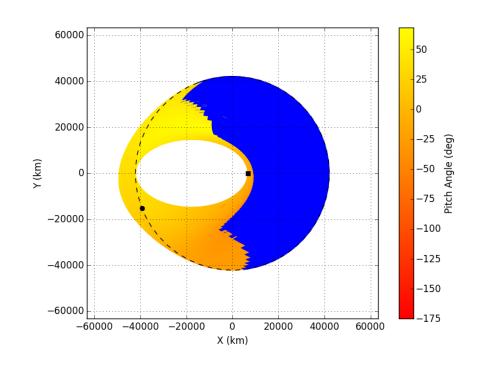




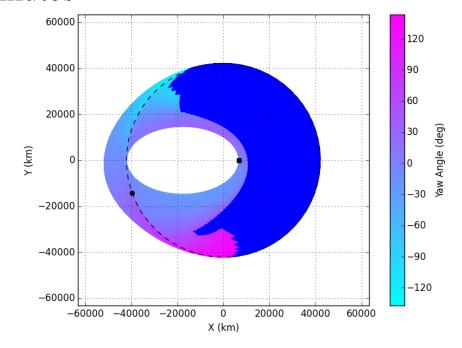


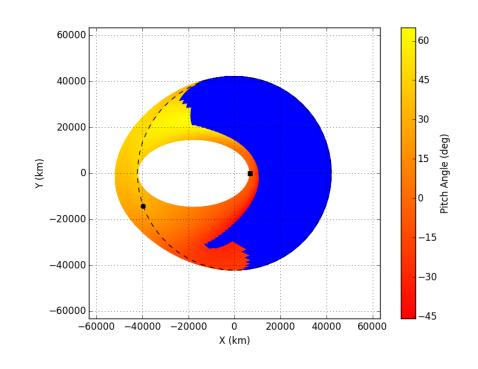
- Choose  $\tau = E$ , the eccentric anomaly
- Minimum fuel GTO to GEO in 450.5 revs
- 2-body dynamics  $+ J_2$
- 135,150 variables
- 61 minutes



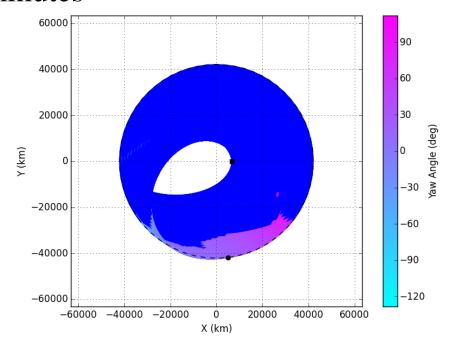


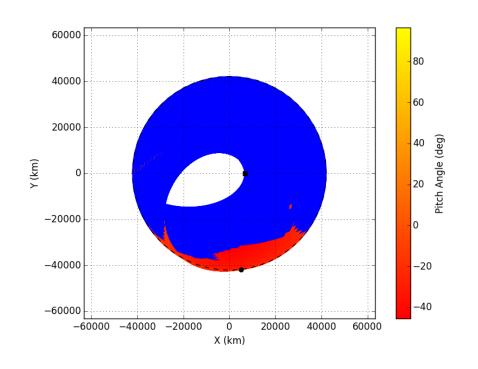
- Choose  $\tau = E$ , the eccentric anomaly
- Minimum fuel GTO to GEO in 450.5 revs
- 2-body dynamics +  $J_2$ + lunar gravity
- 135,150 variables
- 107 minutes





- Choose  $\tau = E$ , the eccentric anomaly
- Minimum fuel GTO to GEO in 1000.5 revs
- 2-body dynamics +  $J_2$ + lunar gravity
- 300,150 variables
- 1359 minutes





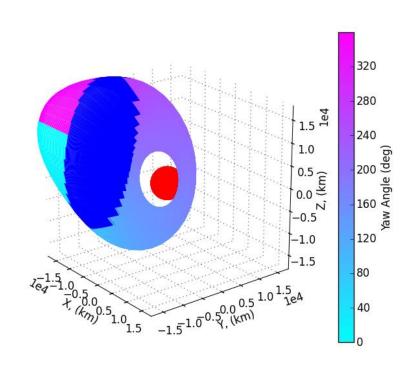


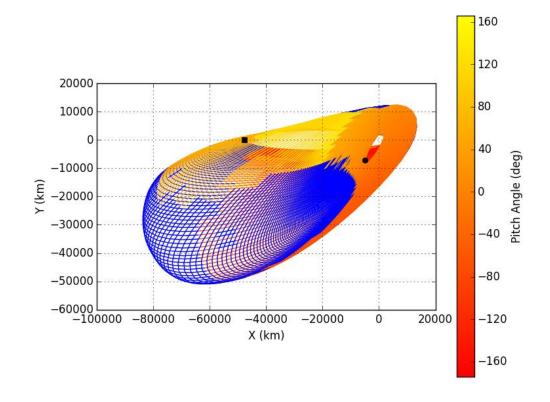
## Backup Slides

Table 2.1: Summary of GTO to GEO Results.

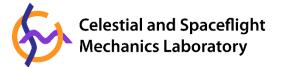
Perturbations	$N_{ m rev}$	Iterations	Runtime (minutes)	$m_f$ (kg)	$t_f$ (days)	$\theta$ (deg)
None	450.5	86	54	1759.1754	315.75	180.0
$J_2$	450.5	111	61	1737.1949	342.13	199.8728
$J_2$ and Lunar Gravity	450.5	136	107	1745.3012	322.63	201.0805
$J_2$ and Lunar Gravity	1000.5	913	1359	1784.3632	558.86	276.7209
None (Eclipse Model)	450.5	93	70	1751.4223	325.48	180.0
None (MEE)	450.5	59	15	1758.7230	318.96	180.0

#### 500 rev orbit lowering at Mars





and with  $\Delta\Omega = 60^{\circ}$ 



## Trust-Region Quadratic Subproblem

- Feedback control laws for  $\delta u$ ,  $\delta \lambda$ ,  $\delta w$  are unconstrained
- Likely to step beyond validity of quadratic expansion
- Require invertible, positive definite Hessians (negative definite for  $J_{\lambda\lambda}$ )
- Trust-region quadratic subproblem (TRQP):

$$\min_{\delta \boldsymbol{u}_k} [J_{u,k}^T \delta \boldsymbol{u}_k + \frac{1}{2} \delta \boldsymbol{u}_k^T J_{uu,k} \delta \boldsymbol{u}_k]$$
s.t.  $\|D \delta \boldsymbol{u}_k\| \leq \Delta$ 

• Acceptance of an iterate:

$$\rho = \frac{\delta J}{ER_{0,0}} \qquad \Delta_{p+1} = \begin{cases} \min((1+\kappa)\Delta_p, \Delta_{\max}), & \text{if } \rho \in [1-\epsilon_1, 1+\epsilon_1] \\ \max((1-\kappa)\Delta_p, \Delta_{\min}), & \text{otherwise} \end{cases}$$



$$X = \begin{bmatrix} t & x & y & z & \dot{x} & \dot{y} & \dot{z} & m & T & \alpha & \beta \end{bmatrix}^{T}$$
 (2)

$$\begin{bmatrix} \hat{r} & \hat{s} & \hat{w} \end{bmatrix} = \begin{bmatrix} \frac{r}{r} & \frac{(r \times v) \times r}{\|(r \times v) \times r\|} & \frac{r \times v}{\|r \times v\|} \end{bmatrix}.$$
(3)

$$\begin{bmatrix} T_r \\ T_s \\ T_w \end{bmatrix} = \begin{bmatrix} T \sin \alpha \cos \beta \\ T \cos \alpha \cos \beta \\ T \sin \beta \end{bmatrix}, \quad \begin{bmatrix} T_x \\ T_y \\ T_z \end{bmatrix} = \begin{bmatrix} \hat{r} & \hat{s} & \hat{w} \end{bmatrix} \begin{bmatrix} T_r \\ T_s \\ T_w \end{bmatrix}, \tag{4}$$

$$\dot{X} = \dot{X}_{\oplus} + \dot{X}_T + \dot{X}_{J_2} + \dot{X}_{\varsigma}, \tag{5}$$

$$\dot{\boldsymbol{X}}_{\oplus} = \begin{bmatrix} 1 & \dot{x} & \dot{y} & \dot{z} & -\frac{\mu_{\oplus}}{r^3} x & -\frac{\mu_{\oplus}}{r^3} y & -\frac{\mu_{\oplus}}{r^3} z & 0 & 0 & 0 \end{bmatrix}^{T}, \tag{6a}$$

$$\dot{X}_{T} = \begin{bmatrix} 0 & 0 & 0 & 0 & \frac{T_{x}}{m} & \frac{T_{y}}{m} & \frac{T_{z}}{m} & -\frac{T}{I_{sp}g_{0}} & 0 & 0 & 0 \end{bmatrix}^{T}, \tag{6b}$$

$$\dot{X}_{J_2} = -\frac{3J_2\mu_{\oplus}R_{\oplus^2}}{2r^5} \begin{bmatrix} 0 & 0 & 0 & 0 & x(1-5\frac{z^2}{r^2}) & y(1-5\frac{z^2}{r^2}) & z(3-5\frac{z^2}{r^2}) & 0 & 0 & 0 \end{bmatrix}^T, \tag{6c}$$

$$\dot{\boldsymbol{X}}_{\mathbf{c}} = -\mu_{\mathbf{c}} \begin{bmatrix} 0 & 0 & 0 & 0 & \frac{x - x_{\mathbf{c}}}{\|\boldsymbol{r} - \boldsymbol{r}_{\mathbf{c}}\|^3} + \frac{x_{\mathbf{c}}}{r_{\mathbf{c}}^3} & \frac{y - y_{\mathbf{c}}}{\|\boldsymbol{r} - \boldsymbol{r}_{\mathbf{c}}\|^3} + \frac{y_{\mathbf{c}}}{r_{\mathbf{c}}^3} & \frac{z - z_{\mathbf{c}}}{\|\boldsymbol{r} - \boldsymbol{r}_{\mathbf{c}}\|^3} + \frac{z_{\mathbf{c}}}{r_{\mathbf{c}}^3} & 0 & 0 & 0 \end{bmatrix}^{T}. \quad (6d)$$

$$\dot{\mathbf{X}} = (\dot{\mathbf{X}}_{\oplus} + \dot{\mathbf{X}}_{T} + \dot{\mathbf{X}}_{J_{2}} + \dot{\mathbf{X}}_{\mathfrak{C}})\sqrt{a/\mu_{\oplus}} r \tag{15}$$

$$A^{i,j} = \frac{\partial \dot{X}^i}{\partial X^j} \,, \tag{16a}$$

$$A^{i,jk} = \frac{\partial^2 \dot{X}^i}{\partial X^j \partial X^k} \,, \tag{16b}$$

$$\Lambda^{i,j} = \frac{\partial \mathring{X}^i}{\partial X^j} \tag{17a}$$

$$\Lambda^{i,jk} = \frac{\partial^2 \mathring{X}^i}{\partial X^j \partial X^k}$$

$$\eta = dt/d\tau = c_n r^n \tag{18}$$

$$\eta_X{}^i = \frac{\partial \eta}{\partial X^i} \tag{19}$$

$$\eta_{XX}{}^{i,j} = \frac{\partial^2 \eta}{\partial X^i \partial X^j}$$

$$\Lambda^{i,j} = A^{i,j} \eta + \dot{X}^i \eta_X^{\ j}$$

$${\it \Lambda}^{i,jk} = {\it A}^{i,jk} \eta + {\it A}^{i,j} \eta_{{\it X}}{}^k + {\it A}^{i,k} \eta_{{\it X}}{}^j + \dot{X}^i \eta_{{\it X}{\it X}}{}^{j,k}$$

$$\Phi^{i,a}(t_k, t_{k+1}) = \frac{\partial \boldsymbol{X}_{k+1}^i}{\partial \boldsymbol{X}_k^a} = \boldsymbol{F}_{X,k}^{i,a}$$

$$\Phi^{i,ab}(t_k, t_{k+1}) = \frac{\partial^2 \boldsymbol{X}_{k+1}^i}{\partial \boldsymbol{X}_k^a \partial \boldsymbol{X}_k^b} = \boldsymbol{F}_{XX,k}^{i,ab}$$

$$\dot{\Phi}^{i,a} = A^{i,\gamma_1}\Phi^{\gamma_1,a}$$

$$\dot{\Phi}^{i,ab} = A^{i,\gamma_1} \Phi^{\gamma_1,ab} + A^{i,\gamma_1\gamma_2} \Phi^{\gamma_1,a} \Phi^{\gamma_2,b}$$

$$A^{i,a} = \frac{\partial X^i}{\partial X^a}$$

$$A^{i,ab} = \frac{\partial^2 \dot{X}^i}{\partial X^a \partial X^b}$$

(21a) 
$$\mathring{\Phi}^{i,j} = \Lambda^{i,a} \Phi^{a,j}$$

(21b) 
$$\dot{\Phi}^{i,jk} = \Lambda^{i,a}\Phi^{a,jk} + \Lambda^{i,ab}\Phi^{a,j}\Phi^{b,k}$$
 (27b)

(27a)

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(17b)

(20)